# Viscosity and Thermal Conductivity of Binary *n*-Heptane + *n*-Alkane Mixtures

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New absolute measurements of the viscosity of binary mixtures of *n*-heptane with *n*-hexane and *n*-nonane are presented. The measurements, performed in a vibrating-wire instrument, cover a temperature range 290–335 K and pressures up to 75 MPa. The concentrations studied are 40 and 70% by weight of *n*-heptane. The accuracy of the reported viscosity data is estimated to be  $\pm 0.5\%$ . The present measurements, together with other *n*-heptane + *n*-alkane viscosity and thermal-conductivity measurements, are used to develop a consistent semiempirical scheme for the correlation and prediction of these mixture properties from those of the pure components.

**KEY WORDS:** *n*-heptane; *n*-nonane; prediction; thermal conductivity; vibrating wire; viscosity.

# **1. INTRODUCTION**

In recent years, semiempirical schemes [1-3] based on considerations of the exact hard-sphere theory of transport properties have been applied for the correlation and prediction of the transport properties. For the liquid *n*-alkanes it has been shown [4] that the thermal conductivity, viscosity, and self-diffusion coefficients can, simultaneously, be successfully correlated over a temperature range 100-400 K and pressures up to 600 MPa, with an accuracy of  $\pm 6$ %. In the case of the transport properties of mixtures, a similar scheme [5, 6] has been applied for the correlation of the thermal conductivity of various binary liquid mixtures at atmospheric pressure, by adopting a simple mixing rule. It has thus recently been shown [7] that, according to this mixing rule, from atmospheric-pressure viscosity measure-

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ments of *n*-heptane + n-undecane, high-pressure viscosity measurements as well as the thermal conductivity of these mixtures can be predicted with an accuracy of  $\pm 3\%$ .

In this paper, new absolute measurements of the viscosity of binary mixtures of *n*-heptane with *n*-hexane and *n*-nonane are presented. At atmospheric pressure, the viscosity measurements cover a temperature range 295-335 K, while at 303.15 and 323.15 K the measurements extend

| Pressure<br>P<br>(MPa) | Temp.<br>T<br>(K) | Density<br>$\rho(T, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T, P)$<br>$(\mu Pa \cdot s)$ | Density<br>$\rho(T_{\text{nom}}, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T_{nom}, P)$<br>$(\mu Pa \cdot s)$ |
|------------------------|-------------------|--|--|---|--|
|                        |                   |  |  | $T_{nom} = 1$   | 303.15 K   |
| 0.10                   | 303.332           | 660.2  | 316.7  | 660.4   | 317.2  |
| 5.57                   | 303.332           | 665.5  | 334.6  | 665.6   | 335.1  |
| 10.54                  | 303.314           | 670.0  | 351.7  | 670.2   | 352.2  |
| 15.60                  | 303.314           | 674.5  | 368.6  | 674.6   | 369.1  |
| 20.67                  | 303.292           | 678.8  | 386.7  | 678.9   | 387.2  |
| 25.74                  | 303.286           | 682.9  | 403.9  | 683.0   | 404.3  |
| 30.90                  | 303.314           | 687.0  | 421.5  | 687.1   | 422.0  |
| 35.87                  | 303.268           | 690.8  | 438.9  | 690.8   | 439.4  |
| 40.94                  | 303.274           | 694.4  | 457.2  | 694.5   | 457.6  |
| 46.00                  | 303.280           | 698.0  | 475.9  | 698.1   | 476,4  |
| 51.17                  | 303.301           | 701.5  | 493.6  | 701.6   | 494.1  |
| 55.83                  | 303.307           | 704.5  | 510.5  | 704.6   | 511.2  |
| 61.20                  | 303.295           | 707.9  | 530.3  | 708.0   | 531.0  |
| 65.96                  | 303.280           | 710.8  | 547.5  | 710.9   | 548.1  |
| 71.74                  | 303.298           | 714.2  | 569.2  | 714.3   | 569.9  |
|                        |                   |  |  | $T_{\rm nom} = 2$   | 323.15 K   |
| 0.10                   | 323.144           | 642.4  | 262.9  | 642.4   | 262.9  |
| 5.38                   | 323.150           | 648.1  | 278.6  | 648.1   | 278.6  |
| 10.44                  | 323.156           | 653.3  | 294.1  | 653.3   | 294.1  |
| 15.50                  | 323.162           | 658.3  | 309.3  | 658.3   | 309.3  |
| 20.77                  | 323.184           | 663.3  | 325.1  | 663.3   | 325.2  |
| 25.74                  | 323.205           | 667.8  | 339.6  | 667.8   | 339.8  |
| 30.80                  | 323.208           | 672.2  | 355.0  | 672.2   | 355.2  |
| 35.77                  | 323.205           | 676.3  | 369.8  | 676.3   | 370.0  |
| 40.83                  | 323.196           | 680.3  | 385.0  | 680.3   | 385.1  |
| 45.70                  | 323.184           | 683.9  | 399.6  | 684.0   | 399.7  |
| 50.76                  | 323.193           | 687.6  | 415.6  | 687.6   | 415.8  |
| 56.03                  | 323.174           | 691.2  | 430.8  | 691.2   | 430.9  |
| 60.90                  | 323.159           | 694.4  | 445.7  | 694.4   | 445.7  |
| 64.24                  | 323.132           | 696.6  | 455.2  | 696.6   | 455.1  |

**Table I.** Viscosity of *n*-Heptane + *n*-Hexane Mixtures as a Function of Pressure (40%, by Weight, of *n*-Heptane)

up to 75 MPa. Moreover, in a recent paper [7] viscosity measurements of n-heptane + n-undecane have been reported. The thermal conductivity of binary mixtures of n-heptane with n-undecane and n-hexadecane has also been reported [8] at atmospheric pressure, over a temperature range 285–350 K. Therefore, these binary mixtures can be used for the examination of the application of the aforementioned scheme to the prediction of the thermal conductivity and viscosity of mixtures.

# 2. EXPERIMENTAL

The viscosity measurements were performed with the high-pressure vibrating-wire instrument described in detail elsewhere [9]. The viscosity of

| Pressure<br>P<br>(MPa) | Temp.<br>T<br>(K) | Density<br>$\rho(T, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T, P)$<br>$(\mu Pa \cdot s)$ | Density<br>$\rho(T_{\text{nom}}, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T_{\text{nom}}, P)$<br>$(\mu \text{Pa} \cdot s)$ |
|------------------------|-------------------|--|--|---|--|
|                        | <u> </u>          |  |  | $T_{\rm nom} = 3$   | 303.15 K   |
| 0.10                   | 303.176           | 667.9  | 343.9  | 667.9   | 344.0  |
| 5.37                   | 303.198           | 672.8  | 363.3  | 672.8   | 363.5  |
| 10.54                  | 303.204           | 677.4  | 382.0  | 677.5   | 382.2  |
| 15.50                  | 303.204           | 681.7  | 400.7  | 681.7   | 400.9  |
| 20.67                  | 303.216           | 686.0  | 421.0  | 686.0   | 421.2  |
| 25.74                  | 303.192           | 690.1  | 440.3  | 690.1   | 440.5  |
| 30.80                  | 303.182           | 694.0  | 459.1  | 694.1   | 459.2  |
| 35.97                  | 303,198           | 697.9  | 479.6  | 698.0   | 479.8  |
| 41.14                  | 303.204           | 701.7  | 500.1  | 701.7   | 500.3  |
| 46.10                  | 303.201           | 705.2  | 519.2  | 705.2   | 519.5  |
| 51.07                  | 303.198           | 708.5  | 539.2  | 708.6   | 539.4  |
| 56.13                  | 303.195           | 711.9  | 559.7  | 711.9   | 559.9  |
| 61.71                  | 303.204           | 715.3  | 583.0  | 715.4   | 583.3  |
|                        |                   |  |  | $T_{\rm nom} = 3$   | 323.15 K   |
| 0.10                   | 323.226           | 650.6  | 283.9  | 650.7   | 284.2  |
| 5.57                   | 323.177           | 656.3  | 301.4  | 656.3   | 301.5  |
| 10.54                  | 323.190           | 661.4  | 317.8  | 661.4   | 317.9  |
| 15.60                  | 323.226           | 666.3  | 334.0  | 666.4   | 334.3  |
| 20.57                  | 323.177           | 671.0  | 351.0  | 671.1   | 351.1  |
| 25.74                  | 323.184           | 675.7  | 367.7  | 675.7   | 367.8  |
| 30.70                  | 323.202           | 679.9  | 383.0  | 680.0   | 383.2  |
| 35.77                  | 323.205           | 684.1  | 399.9  | 684.1   | 400.2  |
| 40.94                  | 323.208           | 688.1  | 417.0  | 688.1   | 417.2  |
| 46.00                  | 323.202           | 691.8  | 433.8  | 691.9   | 434.0  |
| 52.99                  | 323.196           | 696.7  | 457.0  | 696.7   | 457.2  |

**Table II.** Viscosity of *n*-Heptane + n-Hexane Mixtures as a Function of Pressure (70%, by Weight, of *n*-Heptane)

toluene was measured before and after each liquid to assure the continuing good operation of the instrument. The accuracy of the measurements is estimated to be  $\pm 0.5$ %' an estimate confirmed by the measurements of the viscosity of toluene [9]. The samples of *n*-hexane, *n*-hexane, and *n*-nonane were all supplied by BDH Chemicals Ltd., with nominal purities better than 99.0, 99.5, and 99.0%, respectively. The density values of *n*-hexane used where those of Dymond et al. [10], while in the case of *n*-heptane and *n*-nonane, density values were obtained from Doolittle [11]. The density of

| $\begin{array}{c c c c c c c c c c c c c c c c c c c $   |       | T unction o | I Flessule (40 /6 | , oy wongin, o | r <i>n</i> moptano)    |                       |
|--|-------|-------------|-------------------|----------------|------------------------|-----------------------|
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $   | Р     | $T^{-}$     | $\rho(T, P)$      | $\mu(T, P)$    | $\rho(T_{\rm nom}, P)$ | $\mu(T_{\rm nom}, P)$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | . ,   | . ,         |                   |                |                        |                       |
| 5.57         303.198         700.5         531.1         700.5         531.4           10.54         303.152         704.6         558.3         704.6         558.3           15.50         303.146         708.5         587.2         708.5         587.2           20.67         303.170         712.4         617.0         712.4         617.1           25.74         303.198         716.2         645.8         716.2         646.1           30.90         303.228         719.9         675.4         719.9         675.7           35.97         303.182         723.5         706.8         723.5         707.0           41.14         303.176         727.0         739.3         727.0         739.5           46.10         303.204         730.2         770.3         730.2         770.7           51.17         303.204         733.4         802.0         733.4         802.4           56.24         303.198         736.5         833.8         736.5         838.4           61.30         303.185         742.3         900.7         742.3         901.0           71.74         303.185         742.3         907.4         745.2 <t< td=""><td></td><td></td><td></td><td></td><td><math>T_{\rm nom} = 3</math></td><td>303.15 K</td></t<> |       |             |                   |                | $T_{\rm nom} = 3$      | 303.15 K              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 0.10  | 303.185     | 695.9             | 499.7          | 696.0                  | 499.9                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 5.57  | 303.198     | 700.5             | 531.1          | 700.5                  | 531.4                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 10.54 | 303.152     | 704.6             | 558.3          | 704.6                  | 558.3                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 15.50 | 303.146     | 708.5             | 587.2          | 708.5                  | 587.2                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 20.67 | 303.170     | 712.4             | 617.0          | 712.4                  | 617.1                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 25.74 | 303.198     | 716.2             | 645.8          | 716.2                  | 646.1                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 30.90 | 303.228     | 719.9             | 675.4          | 719.9                  | 675.7                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |       |             | 723.5             | 706.8          | 723.5                  | 707.0                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 41.14 | 303.176     | 727.0             | 739.3          | 727.0                  | 739.5                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 46.10 | 303.204     | 730.2             | 770.3          | 730.2                  | 770.7                 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  | 51.17 | 303.204     | 733.4             | 802.0          | 733.4                  | 802.4                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 56.24 | 303.198     | 736.5             | 833.8          | 736.5                  | 834.2                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 61.30 | 303.192     | 739.5             | 868.4          | 739.5                  | 868.8                 |
| $T_{nom} = 323.15 \text{ K}$   | 66.37 | 303.185     | 742.3             | 900.7          | 742.3                  | 901.0                 |
| $            0.10  322.994  680.1  403.2  680.0  402.4 \\            5.22  323.074  684.9  426.8  684.9  426.4 \\            10.54  323.086  689.7  451.8  689.8  451.5 \\            15.50  323.071  694.2  474.8  694.2  474.3 \\            20.57  323.071  698.7  499.1  698.6  498.6 \\            25.53  323.071  702.7  523.0  702.6  522.5 \\            30.50  323.065  706.6  546.5  706.6  546.0 \\            35.87  323.016  714.5  597.5  714.4  596.6 \\            46.00  322.988  717.9  622.6  717.8  621.5 \\            51.07  322.988  721.2  647.9  721.1  646.6 \\            56.03  323.028  727.5  699.9  727.4  698.9 \\            $  | 71.74 | 303.152     | 745.2             | 937.4          | 745.2                  | 937.4                 |
| 5.22 $323.074$ $684.9$ $426.8$ $684.9$ $426.4$ $10.54$ $323.086$ $689.7$ $451.8$ $689.8$ $451.5$ $15.50$ $323.071$ $694.2$ $474.8$ $694.2$ $474.3$ $20.57$ $323.071$ $698.7$ $499.1$ $698.6$ $498.6$ $25.53$ $323.071$ $702.7$ $523.0$ $702.6$ $522.5$ $30.50$ $323.065$ $706.6$ $546.5$ $706.6$ $546.0$ $35.87$ $323.034$ $710.7$ $572.8$ $710.6$ $572.1$ $41.04$ $323.016$ $714.5$ $597.5$ $714.4$ $596.6$ $46.00$ $322.988$ $717.9$ $622.6$ $717.8$ $621.5$ $51.07$ $322.988$ $721.2$ $647.9$ $721.1$ $646.6$ $56.03$ $323.016$ $724.3$ $673.3$ $724.2$ $672.2$ $61.30$ $323.028$ $727.5$ $699.9$ $727.4$ $698.9$   |       |             |                   |                | $T_{\rm nom} = 2$      | 323.15 K              |
| 5.22 $323.074$ $684.9$ $426.8$ $684.9$ $426.4$ $10.54$ $323.086$ $689.7$ $451.8$ $689.8$ $451.5$ $15.50$ $323.071$ $694.2$ $474.8$ $694.2$ $474.3$ $20.57$ $323.071$ $698.7$ $499.1$ $698.6$ $498.6$ $25.53$ $323.071$ $702.7$ $523.0$ $702.6$ $522.5$ $30.50$ $323.065$ $706.6$ $546.5$ $706.6$ $546.0$ $35.87$ $323.034$ $710.7$ $572.8$ $710.6$ $572.1$ $41.04$ $323.016$ $714.5$ $597.5$ $714.4$ $596.6$ $46.00$ $322.988$ $717.9$ $622.6$ $717.8$ $621.5$ $51.07$ $322.988$ $721.2$ $647.9$ $721.1$ $646.6$ $56.03$ $323.016$ $724.3$ $673.3$ $724.2$ $672.2$ $61.30$ $323.028$ $727.5$ $699.9$ $727.4$ $698.9$   | 0.10  | 322.994     | 680.1             | 403.2          | 680.0                  | 402.4                 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |       |             | 684.9             | 426.8          | 684.9                  | 426.4                 |
| 15.50323.071694.2474.8694.2474.320.57323.071698.7499.1698.6498.625.53323.071702.7523.0702.6522.530.50323.065706.6546.5706.6546.035.87323.016714.5597.5714.4596.646.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   |       |             |                   |                | 689.8                  |                       |
| 20.57323.071698.7499.1698.6498.625.53323.071702.7523.0702.6522.530.50323.065706.6546.5706.6546.035.87323.034710.7572.8710.6572.141.04323.016714.5597.5714.4596.646.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   |       |             |                   |                |                        | 474.3                 |
| 30.50323.065706.6546.5706.6546.035.87323.034710.7572.8710.6572.141.04323.016714.5597.5714.4596.646.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 20.57 | 323.071     | 698.7             | 499.1          | 698.6                  | 498.6                 |
| 35.87323.034710.7572.8710.6572.141.04323.016714.5597.5714.4596.646.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 25.53 | 323.071     | 702.7             | 523.0          | 702.6                  | 522.5                 |
| 41.04323.016714.5597.5714.4596.646.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 30.50 | 323.065     | 706.6             | 546.5          | 706.6                  | 546.0                 |
| 46.00322.988717.9622.6717.8621.551.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 35.87 | 323.034     | 710.7             | 572.8          | 710.6                  | 572.1                 |
| 51.07322.988721.2647.9721.1646.656.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 41.04 | 323.016     | 714.5             |                |                        |                       |
| 56.03323.016724.3673.3724.2672.261.30323.028727.5699.9727.4698.9   | 46.00 | 322.988     | 717.9             | 622.6          | 717.8                  | 621.5                 |
| 61.30323.028727.5699.9727.4698.9   | 51.07 | 322.988     | 721.2             | 647.9          | 721.1                  | 646.6                 |
|  | 56.03 | 323.016     | 724.3             | 673.3          | 724.2                  | 672.2                 |
| 66.77 323.104 730.5 726.7 730.5 726.3  | 61.30 | 323.028     | 727.5             | 699.9          | 727.4                  | 698.9                 |
|  | 66.77 | 323.104     | 730.5             | 726.7          | 730.5                  | 726.3                 |

**Table III.** Viscosity of *n*-Heptane + n-Nonane Mixtures as a Function of Pressure (40%, by Weight, of *n*-Heptane)

the mixture was calculated from the densities of the pure components. The mixtures studied, 40 and 70% by weight of *n*-heptane, were prepared gravimetrically and the uncertainty in their composition was less than 0.005%.

# 3. RESULTS

Tables I–IV present the viscosity measurements of the binary mixtures of n-heptane with n-hexane and n-nonane at the measuring temperatures

| Pressure<br>P<br>(MPa) | Temp.<br><i>T</i><br>(K) | Density<br>$\rho(T, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T, P)$<br>$(\mu Pa \cdot s)$ | Density<br>$\rho(T_{\text{nom}}, P)$<br>$(\text{kg} \cdot \text{m}^{-3})$ | Viscosity<br>$\mu(T_{nom}, P)$<br>$(\mu Pa \cdot s)$ |
|------------------------|--------------------------|--|--|---|--|
|                        | <u> </u>                 |  |  | $T_{\rm nom} = 3$   | 303.15 K   |
| 0.10                   | 303.347                  | 685.5  | 432.4  | 685.6   | 433.2  |
| 5.47                   | 303.320                  | 690.2  | 457.7  | 690.3   | 458.4  |
| 10.54                  | 303.307                  | 694.5  | 482.0  | 694.6   | 482.7  |
| 15.50                  | 303.326                  | 698.5  | 506.4  | 698.7   | 507.2  |
| 20.57                  | 303.314                  | 702.6  | 532.1  | 702.7   | 532.9  |
| 25.63                  | 303.311                  | 706.5  | 556.6  | 706.6   | 557.4  |
| 30.70                  | 303.320                  | 710.3  | 581.6  | 710.4   | 582.5  |
| 35.87                  | 303.314                  | 714.0  | 607.4  | 714.1   | 608.3  |
| 40.23                  | 303.323                  | 717.1  | 630.0  | 717.2   | 631.0  |
| 46.10                  | 303.320                  | 721.1  | 660.2  | 721.2   | 661.2  |
| 51.07                  | 303.332                  | 724.3  | 685.9  | 724.5   | 687.0  |
| 56.13                  | 303.332                  | 727.6  | 713.4  | 727.7   | 714.5  |
| 61.30                  | 303.314                  | 730.7  | 742.0  | 730.8   | 743.1  |
| 66.27                  | 303.298                  | 733.6  | 767.7  | 733.7   | 768.8  |
| 71.84                  | 303.365                  | 736.6  | 797.5  | 736.8   | 799.0  |
|                        |                          |  |  | $T_{\rm nom} = 3$   | 323.15 K   |
| 0.10                   | 323.138                  | 669.4  | 353.8  | 669.4   | 353.8  |
| 5.27                   | 323.208                  | 674.5  | 374.0  | 674.5   | 374.2  |
| 10.54                  | 323.196                  | 679.5  | 395.1  | 679.5   | 395.3  |
| 15.60                  | 323.138                  | 684.3  | 415.6  | 684.3   | 415.6  |
| 20.67                  | 323.177                  | 688.8  | 436.3  | 688.8   | 436.5  |
| 25.64                  | 323.177                  | 693.1  | 456.7  | 693.1   | 456.8  |
| 30.90                  | 323.220                  | 697.3  | 477.0  | 697.4   | 477.4  |
| 35.87                  | 323.254                  | 701.2  | 497.6  | 701.3   | 498.2  |
| 40.94                  | 323.181                  | 705.0  | 519.7  | 705.1   | 519.9  |
| 46.10                  | 323.184                  | 708.7  | 541.2  | 708.7   | 541.4  |
| 50.97                  | 323.184                  | 711.9  | 562.1  | 712.0   | 562.3  |
| 55.83                  | 323.190                  | 715.0  | 582.0  | 715.1   | 582.3  |
| 57.86                  | 323.190                  | 716.3  | 591.1  | 716.3   | 591.4  |

**Table IV.** Viscosity of *n*-Heptane + n-Nonane Mixtures as a Function of Pressure (70%, by Weight, of *n*-Heptane)

around 303.15 and 323.15 K as a function of pressure. For each binary mixture two compositions were studied, 40 and 70%, by weight, of n-heptane. In these tables we provide also the viscosity adjusted to the nominal temperatures of 303.15 and 323.15 K, respectively, by means of a linear correction. Since, however, this correction is very small, less than 0.2%, the uncertainty introduced with this assumption is negligible. In Table V, the viscosity measurements at atmospheric pressure as a function of temperature are presented.

The viscosity measurements of these mixtures have been correlated with pressure along each isotherm, for the purpose of interpolation only, by a Tait-like equation as

$$\ln\left[\frac{\mu}{\mu_0}\right] = E \ln\left[\frac{D+P}{D+0.1}\right] \tag{1}$$

where  $\mu_0$  represents the experimental viscosity at atmospheric pressure. The values of the constants for each isotherm for both mixtures are shown in Table VI. In the same table, the standard deviation of each fit is shown. It can be seen that the maximum standard deviation is  $\pm 0.15\%$ . In the

|                   | 40 %   |  |                   | 70 %   |  |
|-------------------|--|--|-------------------|--|--|
| Temp.<br>T<br>(K) | Density<br>$\rho$<br>(kg · m <sup>-3</sup> ) | Viscosity<br>$\mu$<br>$(\mu Pa \cdot s)$ | Temp.<br>T<br>(K) | Density<br>$\rho$<br>(kg · m <sup>-3</sup> ) | Viscosity<br>$\mu$<br>$(\mu Pa \cdot s)$ |
|                   |  | <i>n</i> -Heptane +                      | <i>n</i> -Hexane  |  |  |
| 293.353           | 668.8  | 349.7                                    | 288.281           | 680.0  | 403.4                                    |
| 303.332           | 660.2  | 316.7                                    | 294.311           | 675.2  | 377.6                                    |
| 312.261           | 652.3  | 289.8                                    | 297.616           | 672.5  | 364.4                                    |
| 323.144           | 642.4  | 263.0                                    | 303.176           | 667.9  | 343.9                                    |
|                   |  |  | 313.278           | 659.3  | 311.4                                    |
|                   |  |  | 323.226           | 650.6  | 283.8                                    |
|                   |  | <i>n</i> -Heptane +                      | n-Nonane          |  |  |
| 293.746           | 703.2  | 558.5                                    | 293.965           | 692.8  | 480.2                                    |
| 303.185           | 695.9  | 499.7                                    | 303.411           | 685.4  | 432.6                                    |
| 313.128           | 688.1  | 447.9                                    | 312.673           | 678.0  | 391.6                                    |
| 322.994           | 680.1  | 403.2                                    | 323.138           | 669.4  | 353.8                                    |
|                   |  |  | 333.254           | 660.8  | 320.1                                    |

 Table V.
 Viscosity of Mixtures as a Function of Temperature at

 Atmospheric Pressure (Concentrations in Weight Percentage of *n*-Heptane)

same table the constants for our previous measurements of the viscosity of *n*-heptane + *n*-undecane mixtures [7] and of the pure components [12] are also included for comparison purposes. In Figs. 1 and 2 the deviations of the present experimental measurements of the viscosity, from those correlated by Eq. (1), are presented. It can be seen that the maximum deviation is less than  $\pm 0.2\%$ .

The atmospheric-pressure measurements of both mixtures have also been correlated, for the purpose of interpolation only, by an equation of the form

$$\mu = A e^{B/T} \tag{2}$$

Temp. Conc. Ε D  $\sigma$  $\mu_0$ (%)  $(\mu Pa \cdot s)$ (-)(MPa) (%) (K) n-Heptane + n-Hexane 303.15 40 1.242  $\pm 0.06$ 317.16 118.7 70 344.00 1.282 121.0 +0.07 $\pm 0.04$ 100 370.70 1.398 133.2 323.15 40 0.995 262.94 86.9  $\pm 0.07$ 70 284.17 1.050 92.4  $\pm 0.07$ 100 304.07 1.264 114.9  $\pm 0.08$ *n*-Heptane + *n*-Nonane 303.15 0 617.03 2.564 242.2  $\pm 0.14$ 40 1.485 +0.10499.90 135.9 70 433.15 1.329 122.4  $\pm 0.08$ 100 370.70 1.398 133.2  $\pm 0.04$ 323.15 0 486.89 1.641 148.9 +0.1140 402.40  $\pm 0.07$ 1.207 105.6 70 353.78 1.190 106.9  $\pm 0.06$ 100 304.07 1.264 114.9  $\pm 0.08$ n-Heptane + n-Undecane 303.15 990.53 2.916 0 256.3  $\pm 0.09$ 40 635.93 1.982 183.8 +0.1570 487.81 1.536 142.9 +0.06100 370.70  $\pm 0.04$ 1.398 133.2 323.15 747.23 179.4 0 2.055 +0.0740 153.8 500.12 1.691  $\pm 0.09$ 70 393.52 1.326 119.4  $\pm 0.05$ 100 304.07 114.9  $\pm 0.08$ 1.264

Table VI.Coefficients of Eq. (1) (Concentrations in<br/>Weight Percentage of *n*-Heptane)

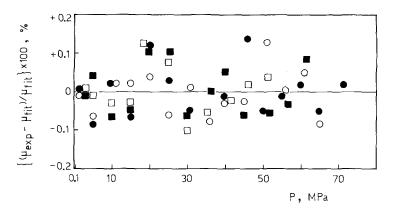


Fig. 1. Deviations of present experimental values of the viscosity of *n*-heptane + *n*-hexane mixtures from Eq. (1). 40%, by weight, of *n*-heptane: ( $\bigcirc$ ) 303.15 K; ( $\bigcirc$ ) 323.15 K. 70%, by weight, of *n*-heptane: ( $\blacksquare$ ) 303.15 K; ( $\Box$ ) 323.15 K.

The values of the constants are shown in Table VII. In the same table, the standard deviation of each fit is shown. It can be seen that the maximum standard deviation is  $\pm 0.19$ %. Also shown for comparison purposes, are the constants for our previous measurements of the viscosity *n*-heptane + *n*-undecane mixtures [7] and of the pure components [12].

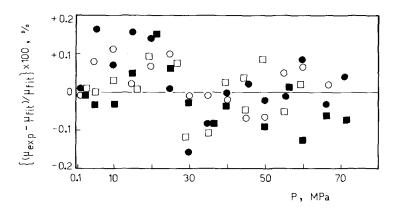


Fig. 2. Deviations of present experimental values of the viscosity of *n*-heptane + *n*-nonane mixtures from Eq. (1). 40%, by weight, of *n*-heptane: ( $\bigcirc$ ) 303.15 K; ( $\bigcirc$ ) 323.15 K. 70%, by weight, of *n*-heptane: ( $\blacksquare$ ) 303.15 K; ( $\Box$ ) 323.15 K.

| Conc.<br>(%) | $\begin{array}{c} A\\ (\mu \mathrm{Pa} \cdot \mathrm{s}) \end{array}$ | В<br>(К)             | σ<br>(%)      |
|--------------|---|----------------------|---------------|
|              | <i>n</i> -Heptan  | e + n-Hexane         |               |
| 40           | $15.75 \pm 0.33$  | $909.7 \pm 6.3$      | $\pm 0.12$    |
| 70           | $15.62 \pm 0.03$  | $937.4 \pm 0.8$      | $\pm 0.02$    |
| 100          | $15.20 \pm 0.18$  | $968.3\pm3.8$        | $\pm 0.03$    |
|              | n-Heptan  | e + n-Nonane         |               |
| 0            | $13.43 \pm 0.03$  | $1160.2\pm0.6$       | $\pm 0.01$    |
| 40           | $15.34 \pm 0.22$  | $1056.2 \pm 4.3$     | $\pm 0.08$    |
| 70           | $15.55\pm0.35$  | $1008.8\pm6.9$       | <u>+</u> 0.19 |
| 100          | $15.20\pm0.18$  | $968.3 \pm 3.8$      | $\pm 0.03$    |
|              | n-Heptane   | + <i>n</i> -Undecane |               |
| 0            | $11.05\pm0.35$  | $1362.4 \pm 9.9$     | $\pm 0.17$    |
| 40           | $13.02 \pm 0.27$  | $1179.2 \pm 6.6$     | $\pm 0.19$    |
| 70           | $15.23 \pm 0.19$  | $1050.5 \pm 4.0$     | $\pm 0.10$    |
| 100          | $15.20 \pm 0.18$  | 968.3 + 3.8          | $\pm 0.03$    |

Table VII.Coefficients of Eq. (2) (Concentrations in<br/>Weight Percentage of *n*-Heptane)

# 4. DISCUSSION

## 4.1. The Pure Liquids

Whereas the correlations of Eqs. (1) and (2) are suitable for interpolation, they have little or no value for extrapolation and prediction. For such purposes it has been shown [4] that a correlation in terms of the molar volume, V, is much more suitable. The hard-sphere model of the dense fluid state [2] suggests the form of such a correlation since it leads to the result that for a monatomic fluid the quantities,  $\mu^*$  and  $\lambda^*$ , defined by the equations

$$\mu^* = 6.035 \times 10^8 \left[ \frac{1}{MRT} \right]^{1/2} \mu V^{2/3} = F_{\mu}(V/V_0)$$
(3)

$$\lambda^* = 1.936 \times 10^7 \left[ \frac{M}{RT} \right]^{1/2} \lambda V^{2/3} = F_{\lambda}(V/V_0)$$
(4)

are functions of the reduced molar volume  $(V/V_0)$  only, where  $V_0$  is a characteristic molar volume of the fluid which is but weakly temperature dependent. In the above equations M represents the molar mass, R the

universal gas constant, and T the absolute temperature, and all quantities are in SI units.

Earlier studies have shown that if the results of Eqs. (3) and (4) are carried over to polyatomic fluids, the functions  $F_{\mu}$  and  $F_{\lambda}$  are nearly universal among a large group of liquids, although the functions are not those predicted from the hard-sphere theory [2]. Recently these functions were obtained [4] as a result of a successful attempt of a simultaneous representation of the thermal conductivity, viscosity, and self-diffusion coefficients of liquid *n*-alkanes over the temperature range 100-400 K and pressures up to 600 MPa. In that study, it emerged that it is not the functions  $\mu^*$  and  $\lambda^*$  which are universal, but a slightly modified version of them, namely,

$$\log \frac{\mu^*}{R_{\mu}} = 0.877 - 3.79208 V_r^{-1} + 16.4416 V_r^{-2} - 24.2509 V_r^{-3} + 16.354 V_r^{-4}$$
(5)

$$\log \frac{\lambda^*}{R_{\lambda}} = 1.0655 - 3.538 V_r^{-1} + 12.121 V_r^{-2} - 12.469 V_r^{-3} + 4.562 V_r^{-4}$$
(6)

in which

$$V_r = V/V_0 \tag{7}$$

and where  $R_{\mu}$  and  $R_{\lambda}$  are factors introduced to account for deviations from the behavior of smooth hard spheres. These factors have been correlated [4, 6] as a function of the carbon number C, as

$$R_{\mu} = 0.9858 + 0.0164C + 0.001432C^{2}$$

$$R_{\lambda} = 0.00225C^{3} - 0.0774C^{2} + 1.186C - 4.672$$

$$+ 14.435C^{-1} - 16.009C^{-2} + 6.296C^{-3}$$
(9)

The characteristic molar volume  $V_0$  of the series was also represented in terms of temperature and the carbon number. For *n*-alkanes with carbon numbers in the range  $C_5$ - $C_{16}$ , the representation for  $V_0$  (in m<sup>3</sup>·mol<sup>-1</sup>) is

$$10^{6}V_{0} = 106.677 - 13.655\theta + 1.6266\theta^{2} + (C-6)(18.028 - 1.2\theta)(0.944 + 0.0035C)$$
(10)

where

$$\theta = T/100$$

This scheme, Eqs. (3)–(10), was found to correlate and predict the viscosity and thermal conductivity of *n*-alkanes in the temperature range 100–400 K and pressures up to 600 MPa, with an accuracy of  $\pm 6\%$ .

### 4.2. The Mixtures

In a recent paper [5] in order to correlate the thermal conductivity of mixtures at atmospheric pressure from the pure components, the following procedure was successfully adopted. It was postulated that the mixture can be considered as an equivalent liquid with a mole fraction average molar mass and a characteristic molar volume  $V_0^{\text{mix}}$ , given by the following mixing rule:

$$V_0^{\rm mix} = XV_0^{\rm I} + (1-X) V_0^{\rm II} - X(1-X)k \tag{11}$$

where  $V_0^{\rm I}$  and  $V_0^{\rm II}$  are the characteristic molar volumes of the pure components, and X the mole fraction. k was found to be a constant characteristic of the pure components, independent of temperature and composition, and determined by experimental measurements. Thus, since the characteristic molar volumes of the pure liquids can be determined by the aforementioned scheme, atmospheric pressure viscosity measurements can be used for the determination of the constant k. Therefore the characteristic molar volume can be calculated and Eqs. (3)-(11) can be used to predict both the viscosity and the thermal conductivity over the whole range of the experimental measurements. The advantage of this scheme is that only one or two measurements at one composition, one temperature, and of one of the two properties at atmospheric pressure, are sufficient to predict both the viscosity and the thermal conductivity of the mixtures over a very wide range of conditions and compositions. This scheme was successfully applied [7] for the prediction of the viscosity and thermal conductivity of n-heptane + n-undecane mixtures.

The present high-pressure viscosity measurements of *n*-heptane with *n*-hexane and *n*-nonane can be used together with our previously reported [7] high-pressure viscosity measurements of *n*-heptane +n-undecane mixtures and the thermal-conductivity measurements of *n*-heptane with *n*-undecane and *n*-hexadecane [8], to examine the power of this scheme. We have thus preferred to slightly modify Eq. (11) in order to cover all these mixtures as

$$V_0^{\rm mix} = XV_0^{\rm I} + (1-X) V_0^{\rm II} - X(1-X) k'(C-7)$$
(12)

where C represents the carbon number of the n-alkane in the n-heptane + n-alkane mixtures. From the atmospheric-pressure viscosity measurements

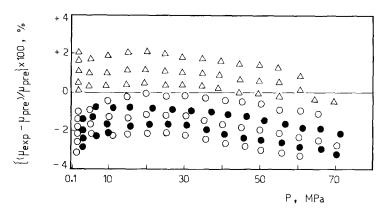


Fig. 3. Deviations of experimental values of the viscosity of *n*-heptane + *n*-alkane mixtures from the scheme of Eqs. (3)-(10) and (12). ( $\bigcirc$ ) *n*-heptane + *n*-hexane mixtures; ( $\bigcirc$ ) *n*-heptane + *n*-nonane mixtures; ( $\triangle$ ) *n*-heptane + *n*-undecane mixtures [7].

of *n*-heptane + *n*-hexane and *n*-heptane + *n*-undecane mixtures, the value of k' was calculated to be equal to  $0.7 \times 10^{-6} \text{ m}^3 \cdot \text{mol}^{-1}$ . Thus, Eqs. (3)–(10) and (12) can be used to calculate the viscosity and the thermal conductivity of all aforementioned mixtures, at any composition, temperature, and pressure (provided the density is available). Figure 3 shows the deviations of the experimental measurements of the viscosity of these mixtures as a function of pressure, from the predicted values, while in Fig. 4 the

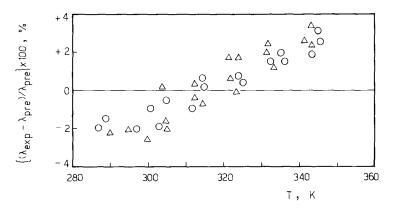


Fig. 4. Deviations of experimental values of the thermal conductivity of n-heptane + n-alkane mixtures from the scheme of Eqs. (3)–(10) and (12). ( $\bigcirc$ ) n-heptane + n-undecane mixtures [8]; ( $\triangle$ ) n-heptane + n-hexadecane mixtures [8].

deviations of the experimental measurements of the thermal conductivity of these mixtures as a function of temperature, from the predicted values, are also shown. It can be seen that in both cases, the maximum deviation is  $\pm 3.5$ %. Thus, the power of this scheme is demonstrated.

# 5. CONCLUSIONS

New absolute measurements of the viscosity of binary mixtures of *n*-heptane with *n*-hexane and *n*-nonane are presented. At atmospheric pressure, the viscosity measurements cover a temperature range 290–335 K, while at 303.15 and 323.15 K the measurements extend up to 75 MPa. The accuracy of the measurements is estimated to be  $\pm 0.5\%$ .

A recently developed semiempirical scheme is applied for the prediction of the viscosity and the thermal conductivity of *n*-heptane + *n*-alkane mixtures over a wide range of compositions and conditions, based only on some atmospheric pressure measurements of the viscosity. The accuracy of this scheme was found to be better than  $\pm 3.5$ %.

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